
APPENDIX B:
Tridiagonal System of Equations

The formulation of many implicit methods for a scalar PDE results in the following equation:

$$a_i^n u_{i-1}^{n+1} + b_i^n u_i^{n+1} + c_i^n u_{i+1}^{n+1} = D_i^n \quad (\text{B-1})$$

Once this equation is applied to all the nodes at the advanced level, a system of linear algebraic equations is obtained. When these equations are represented in a matrix form, the coefficient matrix is tridiagonal. We will take advantage of the tridiagonal nature of the coefficient matrix and review a very efficient solution procedure.

To see the matrix formulation of the equations, consider the Laasonen implicit formulation of our diffusion model equation, i.e., Equation (3-12), presented here as

$$(d)u_{i-1}^{n+1} - (2d + 1)u_i^{n+1} + (d)u_{i+1}^{n+1} = -u_i^n \quad (\text{B-2})$$

where $d = \frac{\alpha \Delta t}{(\Delta x)^2}$ is the diffusion number. Define the following coefficients of (B-2) according to the formulation of (B-1):

$$a = d$$

$$b = -(2d + 1)$$

$$c = d$$

$$D = \text{RHS}$$

Applying Equation (B-2) to all the grid points will result in the following set of linear algebraic equations:

$$i = 2 \quad a_2 u_1 + b_2 u_2 + c_2 u_3 = D_2 \quad (\text{B-3})$$

Note that we have introduced a fictitious boundary at $IMP1 = IM + 1$. The grid points are shown in Figure B-1. Now, at $i = IM$ (the upper boundary), we have

$$a_{IM}u_{IM1} + b_{IM}u_{IM} + c_{IM}u_{IMP1} = D_{IM}$$

or

$$a_{IM}u_{IM1} + (b_{IM} + c_{IM})u_{IM} = D_{IM}$$

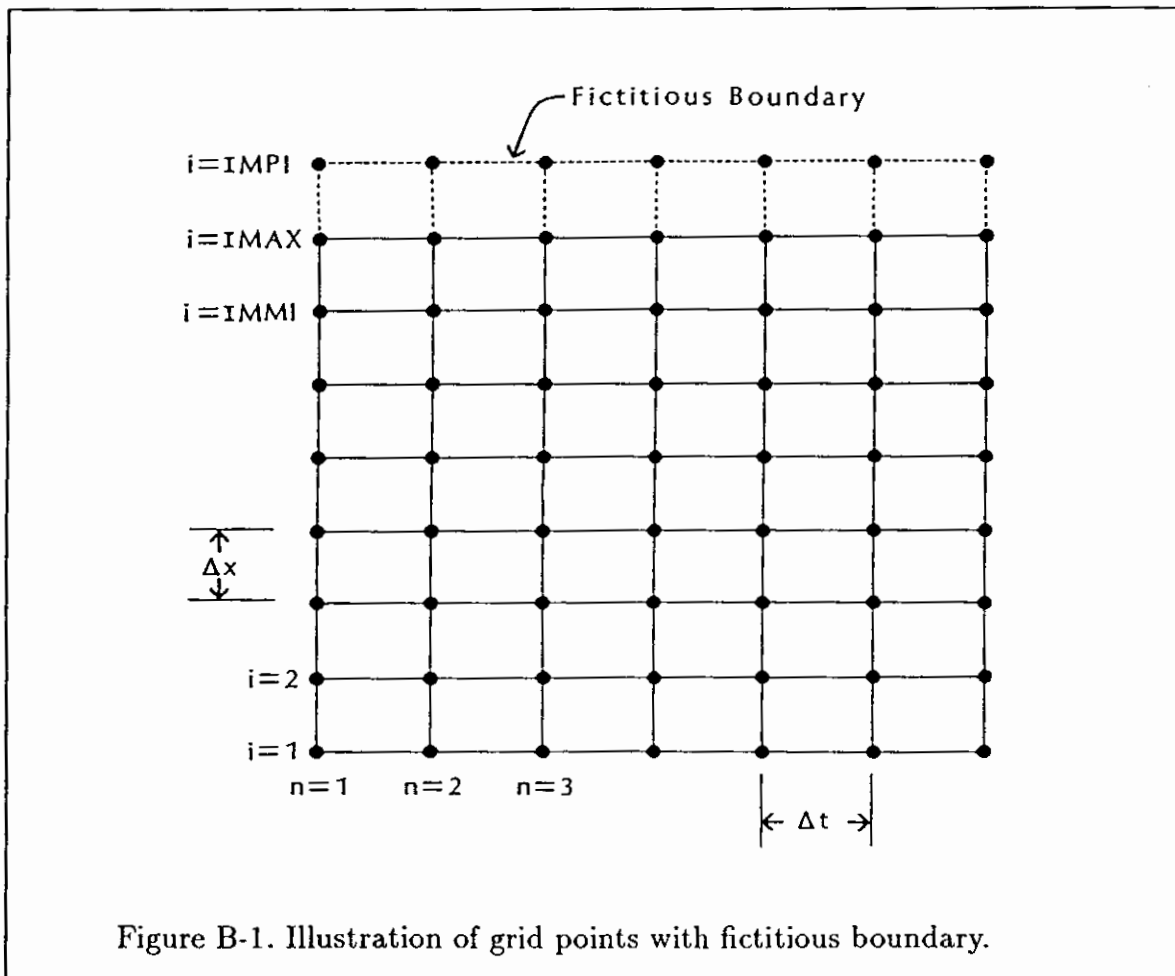


Figure B-1. Illustration of grid points with fictitious boundary.

Comparing Equations (B-7) with (B-5), one concludes that

$$H_i = \frac{c_i}{b_i - a_i H_{i-1}} \quad (\text{B-8})$$

and

$$G_i = \frac{D_i - a_i G_{i-1}}{b_i - a_i H_{i-1}} \quad (\text{B-9})$$

Now that H_i and G_i have been determined, the recursion equation, (B-5), can be used to solve for all the unknowns.

To see how this procedure is applied, consider the parabolic equation investigated in Chapter 3, i.e., the suddenly accelerated plane. At the lower boundary $i = 1$, $u_1 = UWALL$ is specified for all times; therefore, (B-5) at $i = 1$ becomes

$$u_1 = -H_1 u_2 + G_1$$

Since this equation must hold for all u_2 , $H_1 = 0$ and $G_1 = u_1 = UWALL$. With the values of H_1 and G_1 provided from the boundary condition, Equations (B-8) and (B-9) can be solved for the values of H_i and G_i at the second node. Subsequently, (B-8) and (B-9) are sequentially applied to all grid points to obtain the values of H_i and G_i . Note that the computation of H_i and G_i starts from the lower boundary and proceeds upward. Now, Equation (B-5) is used for the computation of u_i . This calculation is performed inward from the upper boundary. At $i = IM$, Equation (B-5) provides

$$u_{IM1} = -H_{IM1} u_{IM} + G_{IM1}$$

In this equation, u_{IM} is specified from the upper boundary condition, with H and G at $IM1$ previously determined. Once u_{IM1} is computed, Equation (B-5) is applied to compute u_{IM2} and so on. The solution procedure may be coded in the program or as a subroutine.

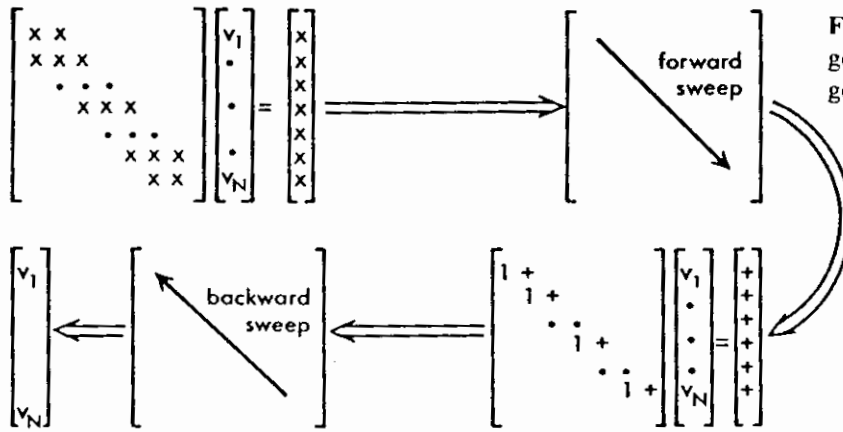


Fig. 6.17. The Thomas algorithm for solving a tridiagonal system of equations.

i.e. the a_i coefficients have been eliminated and the b_i coefficients normalised to unity. For the first equation

$$c'_1 = \frac{c_1}{b_1}, \quad d'_1 = \frac{d_1}{b_1}, \tag{6.29}$$

and for the general equation

$$c'_i = \frac{c_i}{b_i - a_i c'_{i-1}}, \tag{6.30}$$

$$d'_i = \frac{d_i - a_i d'_{i-1}}{b_i - a_i c'_{i-1}}.$$

The equations are modified, as in (6.30), in a forward sweep (Fig. 6.17). The second stage consists of a back-substitution (backward sweep in Fig. 6.17),

$$v_N = d'_N \quad \text{and} \tag{6.31}$$

$$v_i = d'_i - v_{i+1} c'_i.$$

The Thomas algorithm is particularly economical; it requires only $5N - 4$ operations (multiplications and divisions). But to prevent ill-conditioning (and hence round-off contamination) it is necessary that

$$|b_i| > |a_i| + |c_i|.$$

The use of splitting for multidimensional problems (Sect. 8.2) typically generates tridiagonal systems of equations that can be solved efficiently using the Thomas algorithm.

6.2.3 BANFAC/BANSOL: Narrowly Banded Gauss Elimination

When A is narrowly banded subroutines BANFAC and BANSOL are suitable for performing Gauss elimination. Subroutine BANFAC (Fig. 6.18) carries out the

| | |
|----|------|
| 1 | |
| 2 | SUB |
| 3 | C |
| 4 | C |
| 5 | C |
| 6 | C |
| 7 | DIM |
| 8 | IF |
| 9 | C |
| 10 | C |
| 11 | C |
| 12 | NP |
| 13 | DO |
| 14 | JP |
| 15 | B |
| 16 | B |
| 17 | 1 CO |
| 18 | RE |
| 19 | C |
| 20 | C |
| 21 | C |
| 22 | C |
| 23 | 2 NE |
| 24 | DC |
| 25 | J |
| 26 | DC |
| 27 | J |
| 28 | IF |
| 29 | C |
| 30 | C |
| 31 | C |
| 32 | J |
| 33 | B |
| 34 | B |
| 35 | B |
| 36 | G |
| 37 | C |
| 38 | C |
| 39 | C |
| 40 | 3 C |
| 41 | I |
| 42 | I |
| 43 | I |
| 44 | I |
| 45 | I |
| 46 | I |
| 47 | 4 |
| 48 | 5 |
| 49 | |
| 50 | |

forward routine results. For particular cases that is "pentadiagonal" associated with the first sub-coefficient. The p

Time integration of potential temperature equation in the ARPS:

$$\rho^* \frac{\theta^{t+\Delta t} - \theta^{t'}}{\Delta \tau} = - \left[\overline{\rho x_{\xi} y_{\eta} \delta_{\zeta} \theta w} \right] + f_{\theta}' \quad (3.4e)$$

$$f_{\theta}' = -ADVT' + \sqrt{G} D_{\theta}'^{-\Delta t} + \sqrt{G} S_{\theta}' \quad (3.5e)$$

where $ADVT$ is the advection terms, and D_{θ} the diffusion / mixing term.

Note that D_{θ} is evaluated at time level $t-\Delta t$.

3.2.4. Special treatment of vertical mixing

Given the vertical mixing coefficients K_{mv} and K_{Hv} that are based, in the PBL, on the length scale l in Eq.(2.43), vertical turbulent mixing often results in a linear stability constraint more severe than that associated with advection, especially when the vertical resolution is high. This problem is dealt with by using an implicit scheme for the vertical mixing terms, wherein these mixing terms are represented as the weighted average of their values at $t + \Delta t$ and $t - \Delta t$, and the resultant tridiagonal equations are solved as in Eq.(A3). Paegle et al. (1976) showed in a 1-D boundary layer model that the implicit scheme is as accurate as the explicit scheme though much more efficient. In the ARPS, due to the use of mode-splitting scheme for acoustic waves, the implicit treatment of vertical mixing is done in two steps - the mixing terms are first integrated without the acoustic terms, their contributions to the time tendencies are added to the forcing terms which are then used in the small time steps to arrive at the final solution.

Control parameters related to vertically implicit treatment of turbulent mixing in the ARPS (from arps.input):

```

#####
c trbvimp Option for implicit treatment of vertical mixing
c      = 0, vertical explicit (default);
c      = 1, vertical implicit
c
c alfcoef Time average weighting coefficient used
c          in the vertically implicit mixing (default is 1.0)
c
#####

&turbulence
  tmixopt = 4,
  trbisotp = 1,
  tkeopt = 1,
  trbvimp = 1,
  alfcoef = 0.25,
  prantl = 1.0,
  tmixcst = 0.0,
  kmlimit = 1.0,
&END

```

$$\nabla_t u_i^n = \sigma \left[\alpha \nabla_{xx} u_i^{n+1} + (1-\alpha) \nabla_{xx} u_i^n \right]$$

$$alfcoef = 1 - \alpha$$

$alfcoef = 1$ - explicit

$= 0$ - fully implicit

ALSO read:

Durrán: Sec. 3.4.1.

Hoffmann: 4.3 on Diffusion equation
Sec